## DATA SHEET

## TDA8926

Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

Preliminary specification

## Power stage $2 \times 50$ W class-D audio amplifier

## CONTENTS

## 1 FEATURES

2 APPLICATIONS
3 GENERAL DESCRIPTION
4 QUICK REFERENCE DATA
5 ORDERING INFORMATION
6
7
8 FUNCTIONAL DESCRIPTION
8.1 Power stage
8.2 Protection
8.2.1 Overtemperature
8.2.2 Short-circuit across the loudspeaker terminals
8.3 BTL operation

9 LIMITING VALUES
10 THERMAL CHARACTERISTICS
11 QUALITY SPECIFICATION
12 DC CHARACTERISTICS
13 AC CHARACTERISTICS
14 SWITCHING CHARACTERISTICS
14.1 Duty factor

TEST AND APPLICATION INFORMATION
BTL application
Package ground connection
Output power
Reference design
Reference design bill of material
Curves measured in reference design
PACKAGE OUTLINE
SOLDERING
Introduction to soldering through-hole mount packages
Soldering by dipping or by solder wave
Manual soldering
Suitability of through-hole mount IC packages for dipping and wave soldering methods
DATA SHEET STATUS
DEFINITIONS
DISCLAIMERS

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

## 1 FEATURES

- High efficiency (>94\%)
- Operating voltage from $\pm 15$ to $\pm 30 \mathrm{~V}$
- Very low quiescent current
- High output power
- Short-circuit proof across the load, only in combination with controller TDA8929T
- Diagnostic output
- Usable as a stereo Single-Ended (SE) amplifier or as a mono amplifier in Bridge-Tied Load (BTL)
- Electrostatic discharge protection (pin to pin)
- Thermally protected, only in combination with controller TDA8929T.


## 3 GENERAL DESCRIPTION

The TDA8926 is the switching power stage of a two-chip set for a high efficiency class-D audio power amplifier system. The system is split into two chips:

- TDA8926J: a digital power stage in a DBS17P power package
- TDA8929T: the analog controller chip in a SO24 package.

With this chip set a compact $2 \times 50 \mathrm{~W}$ audio amplifier system can be built, operating with high efficiency and very low dissipation. No heatsink is required, or depending on supply voltage and load, a very small one. The system operates over a wide supply voltage range from $\pm 15$ up to $\pm 30 \mathrm{~V}$ and consumes a very low quiescent current.

## 2 APPLICATIONS

- Television sets
- Home-sound sets
- Multimedia systems
- All mains fed audio systems
- Car audio (boosters).


## 4 QUICK REFERENCE DATA

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| General; $\mathrm{V}_{\mathrm{P}}= \pm 25 \mathrm{~V}$ |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{P}}$ | supply voltage |  | $\pm 15$ | $\pm 25$ | $\pm 30$ | V |
| $\mathrm{I}_{\mathrm{q} \text { (tot) }}$ | total quiescent current | no load connected | - | 35 | 45 | mA |
| $\eta$ | efficiency | $\mathrm{P}_{\mathrm{o}}=30 \mathrm{~W}$ | - | 94 | - | \% |
| Stereo single-ended configuration |  |  |  |  |  |  |
| $\mathrm{P}_{0}$ | output power | $\mathrm{R}_{\mathrm{L}}=8 \Omega ; \mathrm{THD}=10 \% ; \mathrm{V}_{\mathrm{P}}= \pm 25 \mathrm{~V}$ | 30 | 37 | - | W |
|  |  | $\mathrm{R}_{\mathrm{L}}=4 \Omega ; \mathrm{THD}=10 \% ; \mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V}$ | 40 | 50 | - | W |
| Mono bridge-tied load configuration |  |  |  |  |  |  |
| $\mathrm{P}_{0}$ | output power | $\mathrm{R}_{\mathrm{L}}=8 \Omega ; \mathrm{THD}=10 \% ; \mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V}$ | 80 | 100 | - | W |

## 5 ORDERING INFORMATION

| TYPE NUMBER | PACKAGE |  |  |
| :--- | :---: | :--- | :--- |
|  | NAME | DESCRIPTION | VERSION |
| TDA8926J | DBS17P | plastic DIL-bent-SIL power package; 17 leads (lead length 12 mm) | SOT243-1 |

> Power stage $2 \times 50$ W class-D audio amplifier

TDA8926

## 6 BLOCK DIAGRAM



Fig. 1 Block diagram.

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

7 PINNING

| SYMBOL | PIN | DESCRIPTION |
| :--- | :---: | :--- |
| SW1 | 1 | digital switch input; channel 1 |
| REL1 | 2 | digital control output; channel 1 |
| DIAG | 3 | digital open-drain output for <br> overtemperature and overcurrent <br> report |
| EN1 | 4 | digital enable input; channel 1 |
| V $_{\text {DD1 }}$ | 5 | positive power supply; channel 1 |
| BOOT1 | 6 | bootstrap capacitor; channel 1 |
| OUT1 | 7 | PWM output; channel 1 |
| VSS1 $^{\text {PW }}$ | 8 | negative power supply; channel 1 |
| STAB | 9 | decoupling internal stabilizer for <br> logic supply |
| VSS2 $^{\text {OUT2 }}$ | 10 | negative power supply; channel 2 |
| OUT | 11 | PWM output; channel 2 |
| BOOT2 | 12 | bootstrap capacitor; channel 2 |
| V $_{\text {DD2 }}$ | 13 | positive power supply; channel 2 |
| EN2 | 14 | digital enable input; channel 2 |
| POWERUP | 15 | enable input for switching on <br> internal reference sources |
| REL2 | 16 | digital control output; channel 2 |
| SW2 | 17 | digital switch input; channel 2 |



Fig. 2 Pin configuration.

# Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier 

## 8 FUNCTIONAL DESCRIPTION

The combination of the TDA8926J and the TDA8929T controller produces a two-channel audio power amplifier system using the class-D technology (see Fig.3). In the TDA8929T controller the analog audio input signal is converted into a digital Pulse Width Modulation (PWM) signal.

The power stage TDA8926 is used for driving the low-pass filter and the loudspeaker load. It performs a level shift from the low-power digital PWM signal, at logic levels, to a high-power PWM signal that switches between the main supply lines. A 2nd-order low-pass filter converts the PWM signal into an analog audio signal across the loudspeaker.

For a description of the controller, see data sheet "TDA8929T, Controller class-D audio amplifier".

### 8.1 Power stage

The power stage contains the high-power DMOS switches, the drivers, timing and handshaking between the power switches and some control logic. For protection, a temperature sensor and a maximum current detector are built-in on the chip.
For interfacing with the controller chip the following connections are used:

- Switch (pins SW1 and SW2): digital inputs; switching from $\mathrm{V}_{\mathrm{SS}}$ to $\mathrm{V}_{\mathrm{SS}}+12 \mathrm{~V}$ and driving the power DMOS switches
- Release (pins REL1 and REL2): digital outputs; switching from $\mathrm{V}_{\mathrm{SS}}$ to $\mathrm{V}_{\mathrm{SS}}+12 \mathrm{~V}$; follow SW1 and SW2 with a small delay
- Enable (pins EN1 and EN2): digital inputs; at a level of $\mathrm{V}_{\mathrm{SS}}$ the power DMOS switches are open and the PWM outputs are floating; at a level of $\mathrm{V}_{\mathrm{SS}}+12 \mathrm{~V}$ the power stage is operational and controlled by the switch pin if pin POWERUP is at $\mathrm{V}_{\mathrm{SS}}+12 \mathrm{~V}$
- Power-up (pin POWERUP): must be connected to a continuous supply voltage of at least $\mathrm{V}_{\mathrm{SS}}+5 \mathrm{~V}$ with respect to $\mathrm{V}_{\mathrm{SS}}$
- Diagnostics (pin DIAG): digital open-drain output; pulled to $\mathrm{V}_{S S}$ if the temperature or maximum current is exceeded.


### 8.2 Protection

Temperature and short-circuit protection sensors are included in the TDA8926. The protection circuits are operational only in combination with the controller TDA8929T. In the event that the maximum current or maximum temperature is exceeded the diagnostic output is activated. The controller has to take appropriate measures by shutting down the system.

### 8.2.1 OVERTEMPERATURE

If the junction temperature $\left(T_{j}\right)$ exceeds $150^{\circ} \mathrm{C}$, then pin DIAG becomes LOW. The diagnostic pin is released if the temperature is dropped to approximately $130^{\circ} \mathrm{C}$, so there is a hysteresis of approximately $20^{\circ} \mathrm{C}$.

### 8.2.2 SHORT-CIRCUIT ACROSS THE LOUDSPEAKER TERMINALS

When the loudspeaker terminals are short-circuited this will be detected by the current protection. If the output current exceeds the maximum output current of 5 A , then pin DIAG becomes LOW. The controller should shut down the system to prevent damage. Using the controller TDA8929T the system is shut down within $1 \mu \mathrm{~s}$, and after 220 ms it will attempt to restart the system again. During this time the dissipation is very low, therefore the average dissipation during a short circuit is practically zero.
7
Fig. 3 Typical application schematic of the class-D system using controller TDA8929T and the TDA8926J.

Fig Typal aplaion

# Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier 

### 8.3 BTL operation

BTL operation can be achieved by driving the audio input channels of the controller in the opposite phase and by connecting the loudspeaker with a BTL output filter between the two outputs (pins OUT1 and OUT2) of the power stage (see Fig.4).

In this way the system operates as a mono BTL amplifier and with the same loudspeaker impedance a four times higher output power can be obtained.

For more information see Chapter 15.


Fig. 4 Mono BTL application.

# Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier 

## 9 LIMITING VALUES

In accordance with the Absolute Maximum Rate System (IEC 60134).

| SYMBOL | PARAMETER | CONDITIONS | MIN. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{P}}$ | supply voltage |  | - | $\pm 30$ | V |
| $\mathrm{V}_{\mathrm{P} \text { (sc) }}$ | supply voltage for short-circuits across the load |  | - | $\pm 30$ | V |
| IORM | repetitive peak current in output pins |  | - | 5 | A |
| $\mathrm{T}_{\text {stg }}$ | storage temperature |  | -55 | +150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {amb }}$ | ambient temperature |  | -40 | +85 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\mathrm{vj}}$ | virtual junction temperature |  | - | 150 | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{V}_{\text {es(HBM) }}$ | electrostatic discharge voltage (HBM) | note 1 <br> all pins with respect to $\mathrm{V}_{\mathrm{DD}}$ (class 1a) all pins with respect to $\mathrm{V}_{S S}$ (class 1a) all pins with respect to each other (class 1a) | $\begin{aligned} & -500 \\ & -1500 \\ & -1500 \end{aligned}$ | $\begin{aligned} & +500 \\ & +1500 \\ & +1500 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |
| $\mathrm{V}_{\text {es(MM) }}$ | electrostatic discharge voltage (MM) | note 2 <br> all pins with respect to $\mathrm{V}_{\mathrm{DD}}$ (class $B$ ) all pins with respect to $\mathrm{V}_{\mathrm{SS}}$ (class B) all pins with respect to each other (class B) | $\begin{aligned} & -250 \\ & -250 \\ & -250 \end{aligned}$ | $\begin{aligned} & +250 \\ & +250 \\ & +250 \end{aligned}$ | $\begin{aligned} & \mathrm{V} \\ & \mathrm{~V} \\ & \mathrm{~V} \end{aligned}$ |

## Notes

1. Human Body Model (HBM); $\mathrm{R}_{\mathrm{s}}=1500 \Omega ; \mathrm{C}=100 \mathrm{pF}$.
2. Machine Model (MM); $\mathrm{R}_{\mathrm{s}}=10 \Omega ; \mathrm{C}=200 \mathrm{pF} ; \mathrm{L}=0.75 \mu \mathrm{H}$.

## 10 THERMAL CHARACTERISTICS

| SYMBOL | PARAMETER | CONDITIONS | VALUE | UNIT |
| :--- | :--- | :--- | :---: | :---: |
| $\mathrm{R}_{\mathrm{th}(\mathrm{j}-\mathrm{a})}$ | thermal resistance from junction to ambient | in free air | 40 | K/W |
| $\mathrm{R}_{\mathrm{th}(\mathrm{j})}$ | thermal resistance from junction to case | in free air | 1.0 | K/W |

## 11 QUALITY SPECIFICATION

In accordance with "SNW-FQ611-part D" if this device is used as an audio amplifier (except for ESD, see also Chapter 9).

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

## 12 DC CHARACTERISTICS

$V_{P}= \pm 25 \mathrm{~V} ; \mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; measured in test diagram of Fig.6; unless otherwise specified.

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Supply |  |  |  |  |  |  |
| $\mathrm{V}_{P}$ | supply voltage | note 1 | $\pm 15$ | $\pm 25$ | $\pm 30$ | V |
| $\mathrm{I}_{\text {(tot) }}$ | total quiescent current | no load connected | - | 35 | 45 | mA |
|  |  | outputs floating | - | 5 | 10 | mA |
| Internal stabilizer logic supply (pin STAB) |  |  |  |  |  |  |
| $\mathrm{V}_{\text {O(STAB) }}$ | stabilizer output voltage |  | 11 | 13 | 15 | V |
| Switch inputs (pins SW1 and SW2) |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{IH}}$ | HIGH-level input voltage | referenced to $\mathrm{V}_{\text {SS }}$ | 10 | - | $\mathrm{V}_{\text {STAB }}$ | V |
| $\mathrm{V}_{\text {IL }}$ | LOW-level input voltage | referenced to $\mathrm{V}_{S S}$ | 0 | - | 2 | V |
| Control outputs (pins REL1 and REL2) |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{OH}}$ | HIGH-level output voltage | referenced to $\mathrm{V}_{\text {SS }}$ | 10 | - | $\mathrm{V}_{\text {STAB }}$ | V |
| $\mathrm{V}_{\text {OL }}$ | LOW-level output voltage | referenced to $\mathrm{V}_{\text {SS }}$ | 0 | - | 2 | V |
| Diagnostic output (pin DIAG, open-drain) |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{OL}}$ | LOW-level output voltage | $\mathrm{I}_{\text {DIAG }}=1 \mathrm{~mA}$; note 2 | 0 | - | 1.0 | V |
| ILO | output leakage current | no error condition | - | - | 50 | $\mu \mathrm{A}$ |
| Enable inputs (pins EN1 and EN2) |  |  |  |  |  |  |
| $\mathrm{V}_{\mathrm{IH}}$ | HIGH-level input voltage | referenced to $\mathrm{V}_{\text {SS }}$ | - | 9 | $\mathrm{V}_{\text {STAB }}$ | V |
| $\mathrm{V}_{\text {IL }}$ | LOW-level input voltage | referenced to $\mathrm{V}_{\text {SS }}$ | 0 | 5 | - | V |
| $\mathrm{V}_{\text {EN(hys) }}$ | hysteresis voltage |  | - | 4 | - | V |
| $\mathrm{I}_{\text {(EN) }}$ | input current |  | - | - | 300 | $\mu \mathrm{A}$ |
| Switching-on input (pin POWERUP) |  |  |  |  |  |  |
| $\mathrm{V}_{\text {POWERUP }}$ | operating voltage | referenced to $\mathrm{V}_{\text {SS }}$ | 5 | - | 12 | V |
| $\mathrm{I}_{\text {(POWERUP) }}$ | input current | $\mathrm{V}_{\text {POWERUP }}=12 \mathrm{~V}$ | - | 100 | 170 | $\mu \mathrm{A}$ |
| Temperature protection |  |  |  |  |  |  |
| $\mathrm{T}_{\text {diag }}$ | temperature activating diagnostic | $\mathrm{V}_{\text {DIAG }}=\mathrm{V}_{\text {DIAG(LOW) }}$ | 150 | - | - | ${ }^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{\text {hys }}$ | hysteresis on temperature diagnostic | $\mathrm{V}_{\text {DIAG }}=\mathrm{V}_{\text {DIAG(LOW }}$ | - | 20 | - | ${ }^{\circ} \mathrm{C}$ |

## Notes

1. The circuit is $D C$ adjusted at $\mathrm{V}_{\mathrm{P}}= \pm 15$ to $\pm 30 \mathrm{~V}$.
2. Temperature sensor or maximum current sensor activated.

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

## 13 AC CHARACTERISTICS

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Single-ended application; note 1 |  |  |  |  |  |  |
| $\mathrm{P}_{0}$ | output power | $\begin{gathered} \mathrm{R}_{\mathrm{L}}=8 \Omega ; \mathrm{V}_{\mathrm{P}}= \pm 25 \mathrm{~V} \\ \mathrm{THD}=0.5 \% \\ \mathrm{THD}=10 \% \\ \mathrm{R}_{\mathrm{L}}=8 \Omega ; \mathrm{V}_{\mathrm{P}}= \pm 30 \mathrm{~V} \\ \mathrm{THD}=0.5 \% \\ \mathrm{THD}=10 \% \\ \mathrm{R}_{\mathrm{L}}=4 \Omega ; \mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V} \\ \mathrm{THD}=0.5 \% \\ \mathrm{THD}=10 \% \end{gathered}$ | $\begin{array}{\|l} 25^{(2)} \\ 30^{(2)} \\ - \\ - \\ 30^{(2)} \\ 40^{(2)} \end{array}$ | $\begin{aligned} & 30 \\ & 37 \\ & 40 \\ & 52 \\ & \\ & 40 \\ & 50 \end{aligned}$ |  | W <br> W <br> W <br> W <br> W <br> W |
| THD | total harmonic distortion | $\begin{aligned} P_{0} & =1 \mathrm{~W} ; \text { note } 3 \\ f_{i} & =1 \mathrm{kHz} \\ f_{i} & =10 \mathrm{kHz} \end{aligned}$ |  | $\begin{aligned} & 0.01 \\ & 0.1 \end{aligned}$ | $0.05$ | $\begin{aligned} & \% \\ & \% \\ & \hline \end{aligned}$ |
| $\mathrm{G}_{\mathrm{v}(\mathrm{cl})}$ | closed-loop voltage gain |  | 29 | 30 | 31 | dB |
| $\eta$ | efficiency | $\mathrm{P}_{\mathrm{o}}=30 \mathrm{~W} ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz}$; note 4 | - | 94 | - | \% |
| Mono BTL application; note 5 |  |  |  |  |  |  |
| $\mathrm{P}_{0}$ | output power | $\mathrm{R}_{\mathrm{L}}=8 \Omega ; \mathrm{THD}=0.5 \%$ | 70 ${ }^{(2)}$ | 80 | - | W |
|  |  | $\mathrm{R}_{\mathrm{L}}=8 \Omega ; \mathrm{THD}=10 \%$ | 80 ${ }^{(2)}$ | 100 | - | W |
| THD | total harmonic distortion | $\begin{gathered} \mathrm{P}_{\mathrm{o}}=1 \mathrm{~W} ; \text { note } 3 \\ \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} \\ \mathrm{f}_{\mathrm{i}}=10 \mathrm{kHz} \end{gathered}$ | - | $\begin{aligned} & 0.01 \\ & 0.1 \end{aligned}$ | $0.05$ | $\begin{aligned} & \% \\ & \% \\ & \hline \end{aligned}$ |
| $\mathrm{G}_{\mathrm{v}(\mathrm{cl})}$ | closed loop voltage gain |  | 35 | 36 | 37 | dB |
| $\eta$ | efficiency | $\mathrm{P}_{\mathrm{o}}=30 \mathrm{~W} ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz}$; note 4 | - | 94 | - | \% |

## Notes

1. $V_{P}= \pm 25 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=8 \Omega ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{f}_{\mathrm{osc}}=310 \mathrm{kHz} ; \mathrm{R}_{\mathrm{S}}=0.1 \Omega$ (series resistance of filter coil); $\mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; measured in reference design (SE application) shown in Fig.7; unless otherwise specified.
2. Indirectly measured; based on $\mathrm{R}_{\mathrm{ds}(\mathrm{on})}$ measurement.
3. Total Harmonic Distortion (THD) is measured in a bandwidth of 22 Hz to 22 kHz . When distortion is measured using a low-order low-pass filter a significantly higher value will be found, due to the switching frequency outside the audio band.
4. Efficiency for power stage; output power measured across the loudspeaker load.
5. $V_{P}= \pm 21 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=8 \Omega ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz} ; \mathrm{f}_{\mathrm{osc}}=310 \mathrm{kHz} ; \mathrm{R}_{\mathrm{S}}=0.1 \Omega$ (series resistance of filter coil); $\mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; measured in reference design (BTL application) shown in Fig.7; unless otherwise specified.

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

## 14 SWITCHING CHARACTERISTICS

$\mathrm{V}_{\mathrm{P}}= \pm 25 \mathrm{~V} ; \mathrm{T}_{\mathrm{amb}}=25^{\circ} \mathrm{C}$; measured in Fig.6; unless otherwise specified.

| SYMBOL | PARAMETER | CONDITIONS | MIN. | TYP. | MAX. | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PWM outputs (pins OUT1 and OUT2); see Fig. 5 |  |  |  |  |  |  |
| $\mathrm{t}_{\mathrm{r}}$ | rise time |  | - | 30 | - | ns |
| $\mathrm{t}_{\mathrm{f}}$ | fall time |  | - | 30 | - | ns |
| $\mathrm{t}_{\text {blank }}$ | blanking time |  | - | 70 | - | ns |
| $t_{\text {PD }}$ | propagation delay | from pin SW1 (SW2) to pin OUT1 (OUT2) | - | 20 | - | ns |
| $\mathrm{t}_{\mathrm{W} \text { (min) }}$ | minimum pulse width | note 1 | - | 220 | 270 | ns |
| $\mathrm{R}_{\mathrm{ds}(\mathrm{on})}$ | on-resistance of the output transistors |  | - | 0.2 | 0.3 | $\Omega$ |

## Note

1. When used in combination with controller TDA8929T, the effective minimum pulse width during clipping is $0.5 \mathrm{t}_{\mathrm{w}(\mathrm{min})}$.

### 14.1 Duty factor

For the practical useable minimum and maximum duty factor ( $\delta$ ) which determines the maximum output power:
$\frac{\mathrm{t}_{\mathrm{W}(\min )} \times \mathrm{f}_{\mathrm{osc}}}{2} \times 100 \%<\delta<\left(1-\frac{\mathrm{t}_{\mathrm{W}(\min )} \times \mathrm{f}_{\mathrm{osc}}}{2}\right) \times 100 \%$
Using the typical values: $3.5 \%<\delta<96.5 \%$.

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

TDA8926


Fig. 5 Timing diagram PWM output, switch and release signals.
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14

Fig. 6 Test diagram.

# Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier 

### 15.1 BTL application

When using the system in a mono BTL application (for more output power), the inputs of both channels of the PWM modulator must be connected in parallel; the phase of one of the inputs must be inverted. In principle the loudspeaker can be connected between the outputs of the two single-ended demodulation filters.

### 15.2 Package ground connection

The heatsink of the TDA8926J is connected internally to $\mathrm{V}_{\mathrm{SS}}$.

### 15.3 Output power

The output power in single-ended applications can be estimated using the formula
$P_{o(1 \%)}=\frac{\left[\frac{R_{L}}{\left(R_{L}+R_{d s(o n)}+R_{s}\right)} \times V_{P} \times\left(1-t_{W(\text { min })} \times f_{o s c}\right)\right]^{2}}{2 \times R_{L}}$
The maximum current $\mathrm{I}_{\mathrm{O}(\max )}=\frac{\left[\mathrm{V}_{\mathrm{P}} \times\left(1-\mathrm{t}_{\mathrm{W}(\min )} \times \mathrm{f}_{\mathrm{osc}}\right)\right]}{\mathrm{R}_{\mathrm{L}}+\mathrm{R}_{\mathrm{ds}(\mathrm{on})}+\mathrm{R}_{\mathrm{s}}}$ should not exceed 5 A .
The output power in BTL applications can be estimated using the formula
$P_{o(1 \%)}=\frac{\left[\frac{R_{L}}{R_{L}+2 \times\left(R_{d s(o n)}+R_{s}\right)} \times 2 V_{P} \times\left(1-t_{W(\text { min })} \times f_{o s c}\right)\right]^{2}}{2 \times R_{L}}$
The maximum current $\mathrm{I}_{\mathrm{O}(\max )}=\frac{\left[2 \mathrm{~V}_{\mathrm{P}} \times\left(1-\mathrm{t}_{\mathrm{W}(\min )} \times \mathrm{f}_{\text {osc }}\right)\right]}{\mathrm{R}_{\mathrm{L}}+2 \times\left(\mathrm{R}_{\mathrm{ds}(\text { on })}+\mathrm{R}_{\mathrm{s}}\right)}$ should not exceed 5 A .
Where:
$R_{L}=$ load impedance
$R_{S}=$ series resistance of filter coil
$\mathrm{P}_{\mathrm{o}(1 \%)}=$ output power just at clipping
The output power at THD $=10 \%: \mathrm{P}_{\mathrm{o}(10 \%)}=1.25 \times \mathrm{P}_{\mathrm{o}(1 \%)}$.

### 15.4 Reference design

The reference design for a two-chip class-D audio amplifier for TDA8926J and controller TDA8929T is shown in Fig.7. The Printed-Circuit Board (PCB) layout is shown in Fig.8. The bill of materials is given in Table 1.

R21 and R22 are necessary only in BTL applications with asymmetrical supply
BTL: remove R6, R7, C23, C26 and C27 and close J5 and J6.
C 22 and C23 influence the low-pass frequency response and should be tuned with the real load (loudspeaker).
Inputs floating or inputs referenced to QGND (close J1 and J4) or referenced to $\mathrm{V}_{\mathrm{SS}}$ (close J 2 and J 3 ) for an input signal ground reference.
Fig. 7 Two-chip class-D audio amplifier application diagram for TDA8926J and controller TDA8929T.
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Silk screen top, top view
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Silk screen bottom, top view


Copper top, top view


Copper bottom, top view
Fig. 8 Printed-circuit board layout for TDA8926J and controller TDA8929T.

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

### 15.5 Reference design bill of material

Table 1 Two-chip class-D audio amplifier PCB (Version 2.1; 03-2001) for TDA8926J and TDA8929T (see Figs 7 and 8)

| COMPONENT | DESCRIPTION | VALUE | COMMENTS |
| :---: | :---: | :---: | :---: |
| $\ln 1$ and $\ln 2$ | Cinch input connectors |  | $2 \times$ Farnell: 152-396 |
| Out1, Out2, $\mathrm{V}_{\mathrm{DD}}$, GND and $V_{S S}$ | supply/output connectors |  | $\begin{aligned} & 2 \times \text { Augat 5KEV-02; } \\ & 1 \times \text { Augat 5KEV-03 } \end{aligned}$ |
| S1 | on/mute/off switch |  | PCB switch Knitter ATE 1 E M-O-M |
| U1 | power stage IC | TDA8926J/27J | DBS17P package |
| U2 | controller IC | TDA8929T | SO24 package |
| L2 and L4 | demodulation filter coils | $33 \mu \mathrm{H}$ | $2 \times$ Sumida CDRH127-330 |
| L5, L6 and L7 | power supply ferrite beads |  | $3 \times$ Murata BL01RN1-A62 |
| C1 and C2 | supply decoupling capacitors for $V_{D D}$ to $V_{S S}$ of the controller | 220 nF/63 V | $2 \times$ SMD1206 |
| C3 | clock decoupling capacitor | $220 \mathrm{nF} / 63 \mathrm{~V}$ | SMD1206 |
| C4 | 12 V decoupling capacitor of the controller | 220 nF/63 V | SMD1206 |
| C5 | 12 V decoupling capacitor of the power stage | $220 \mathrm{nF} / 63 \mathrm{~V}$ | SMD1206 |
| C6 and C7 | supply decoupling capacitors for $V_{D D}$ to $V_{S S}$ of the power stage | 220 nF/63 V | SMD1206 |
| C8 and C9 | bootstrap capacitors | $15 \mathrm{nF} / 50 \mathrm{~V}$ | $2 \times$ SMD0805 |
| $\begin{aligned} & \hline \text { C10, C11, } \\ & \text { C12 and C13 } \end{aligned}$ | snubber capacitors | $560 \mathrm{pF} / 100 \mathrm{~V}$ | $4 \times$ SMD0805 |
| C14 and C16 | demodulation filter capacitors | 470 nF/63 V | $2 \times \mathrm{MKT}$ |
| C15 and C17 | resonance suppress capacitors | $220 \mathrm{nF} / 63 \mathrm{~V}$ | $2 \times$ SMD1206 |
| $\begin{aligned} & \hline \text { C18, C19, } \\ & \text { C20 and C21 } \end{aligned}$ | common mode HF coupling capacitors | $1 \mathrm{nF} / 50 \mathrm{~V}$ | $4 \times$ SMD0805 |
| C22 and C23 | input filter capacitors | $330 \mathrm{pF} / 50 \mathrm{~V}$ | $2 \times$ SMD1206 |
| C24, C25, <br> C26 and C27 | input capacitors | 470 nF/63 V | $4 \times \mathrm{MKT}$ |
| $\begin{aligned} & \hline \text { C28, C29, } \\ & \text { C30 and C31 } \end{aligned}$ | common mode HF coupling capacitors | $1 \mathrm{nF} / 50 \mathrm{~V}$ | $2 \times$ SMD0805 |
| C32 and C33 | power supply decoupling capacitors | $220 \mathrm{nF} / 63 \mathrm{~V}$ | $2 \times$ SMD1206 |
| C34 and C35 | power supply electrolytic capacitors | $1500 \mu \mathrm{~F} / 35 \mathrm{~V}$ | $2 \times$ Rubycon ZL very low ESR (large switching currents) |
| $\begin{aligned} & \hline \text { C36, C37, } \\ & \text { C38 and C39 } \end{aligned}$ | analog supply decoupling capacitors | $220 \mathrm{nF} / 63 \mathrm{~V}$ | $4 \times$ SMD1206 |
| C40 and C41 | analog supply electrolytic capacitors | $47 \mu \mathrm{~F} / 35 \mathrm{~V}$ | $2 \times$ Rubycon ZA low ESR |
| C43 | diagnostic capacitor | $180 \mathrm{pF} / 50 \mathrm{~V}$ | SMD1206 |
| C44 | mode capacitor | 220 nF/63 V | SMD1206 |
| D1 | 5.6 V Zener diode | BZX79C5V6 | DO-35 |
| D2 | 7.5 V Zener diode | BZX79C7V5 | DO-35 |
| R1 | clock adjustment resistor | $27 \mathrm{k} \Omega$ | SMD1206 |

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

| COMPONENT | DESCRIPTION | VALUE | COMMENTS |
| :--- | :--- | :--- | :--- |
| R4, R5, <br> R6 and R7 | input resistors | $10 \mathrm{k} \Omega$ | $4 \times$ SMD1206 |
| R10 | diagnostic resistor | $1 \mathrm{k} \Omega$ | SMD1206 |
| R11, R12, <br> R13 and R14 | snubber resistors | $5.6 \Omega ;>0.25 \mathrm{~W}$ | $4 \times$ SMD1206 |
| R15 and R16 | resonance suppression resistors | $24 \Omega$ | $2 \times$ SMD1206 |
| R19 | mode select resistor | $39 \mathrm{k} \Omega$ | SMD1206 |
| R20 | mute select resistor | $39 \mathrm{k} \Omega$ | SMD1206 |
| R21 | resistor needed when using an <br> asymmetrical supply | $10 \mathrm{k} \Omega$ | SMD1206 |
| R22 | resistor needed when using an <br> asymmetrical supply | $9.1 \mathrm{k} \Omega$ | SMD1206 |
| R24 | bias resistor for powering-up the power <br> stage | $200 \mathrm{k} \Omega$ | SMD1206 |

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

### 15.6 Curves measured in reference design



Fig. 9 Total harmonic distortion plus noise as a function of output power.


Fig. 11 Total harmonic distortion plus noise as a function of output power.


$2 \times 4 \Omega \mathrm{SE} ; \mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V}$.
(1) $\mathrm{P}_{\mathrm{O}}=10 \mathrm{~W}$.
(2) $P_{0}=1 \mathrm{~W}$.

Fig. 12 Total harmonic distortion plus as a function of input frequency.

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier



Fig. 13 Total harmonic distortion plus noise as a function of output power.

$\mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V} ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz}$.
(1) $2 \times 4 \Omega \mathrm{SE}$.
(2) $1 \times 8 \Omega \mathrm{BTL}$.
(3) $2 \times 8 \Omega \mathrm{SE}$.

Fig. 15 Power dissipation as a function of output power.



Fig. 16 Efficiency as a function of output power.

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier


$\mathrm{THD}+\mathrm{N}=0.5 \% ; \mathrm{f}_{\mathrm{i}}=1 \mathrm{kHz}$.
(1) $1 \times 8 \Omega \mathrm{BTL}$.
(2) $2 \times 4 \Omega \mathrm{SE}$.
(3) $2 \times 8 \Omega \mathrm{SE}$.

Fig. 17 Output power as a function of supply voltage.

$2 \times 8 \Omega \mathrm{SE} ; \mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V}$.
(1) $\mathrm{P}_{\mathrm{O}}=10 \mathrm{~W}$.
(2) $P_{0}=1 \mathrm{~W}$.

Fig. 19 Channel separation as a function of input frequency.

$T H D+N=10 \% ; f_{i}=1 \mathrm{kHz}$.
(1) $1 \times 8 \Omega \mathrm{BTL}$.
(2) $2 \times 4 \Omega \mathrm{SE}$.
(3) $2 \times 8 \Omega \mathrm{SE}$.

Fig. 18 Output power as a function of supply voltage.

$2 \times 4 \Omega \mathrm{SE} ; \mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V}$.
(1) $\mathrm{P}_{\mathrm{O}}=10 \mathrm{~W}$.
(2) $P_{0}=1 \mathrm{~W}$.

Fig. 20 Channel separation as a function of input frequency.

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier


$\mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V} ; \mathrm{V}_{\mathrm{i}}=100 \mathrm{mV} ; \mathrm{R}_{\mathrm{s}}=10 \mathrm{k} \Omega / \mathrm{C}_{\mathrm{i}}=330 \mathrm{pF}$.
(1) $1 \times 8 \Omega \mathrm{BTL}$.
(2) $2 \times 8 \Omega \mathrm{SE}$.
(3) $2 \times 4 \Omega \mathrm{SE}$.

Fig. 21 Gain as a function of input frequency.

$\mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V} ; \mathrm{V}_{\text {ripple(p-p) }}=2 \mathrm{~V}$.
(1) Both supply lines in antiphase.
(2) Both supply lines in phase.
(3) One supply line rippled.

Fig. 23 Supply voltage ripple rejection as a function of input frequency.

$\mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V} ; \mathrm{V}_{\mathrm{i}}=100 \mathrm{mV} ; \mathrm{R}_{\mathrm{s}}=0 \Omega$.
(1) $1 \times 8 \Omega \mathrm{BTL}$.
(2) $2 \times 8 \Omega \mathrm{SE}$.
(3) $2 \times 4 \Omega \mathrm{SE}$.

Fig. 22 Gain as a function of input frequency.

$\mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V}$.
(1) $f_{\text {ripple }}=1 \mathrm{kHz}$.
(2) $f_{\text {ripple }}=100 \mathrm{~Hz}$.
(3) $f_{\text {ripple }}=10 \mathrm{~Hz}$.

Fig. 24 Supply voltage ripple rejection as a function of ripple voltage (peak-to-peak value).

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier


$R_{L}=$ open-circuit.
Fig. 25 Quiescent current as a function of supply voltage.

$V_{P}= \pm 21 \mathrm{~V} ; 1500 \mu \mathrm{~F}$ per supply line; $\mathrm{f}_{\mathrm{i}}=10 \mathrm{~Hz}$.
(1) $1 \times 4 \Omega S E$.
(2) $1 \times 8 \Omega \mathrm{SE}$.

Fig. 27 Supply voltage ripple as a function of output power.



## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier


$\mathrm{V}_{\mathrm{P}}= \pm 21 \mathrm{~V} ; \mathrm{P}_{\mathrm{o}}=1 \mathrm{~W}$ in $2 \times 8 \Omega$.
(1) 10 kHz .
(2) 1 kHz .
(3) 100 Hz .

Fig. 29 Total harmonic distortion plus noise as a function of clock frequency.

$\mathrm{V}_{\mathrm{P}}= \pm 25 \mathrm{~V} ; \mathrm{R}_{\mathrm{L}}=$ open-circuit.
Fig. 31 Quiescent current as a function of clock frequency.



Fig. 32 PWM residual voltage as a function of clock frequency.

## Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier

TDA8926

16 PACKAGE OUTLINE
DBS17P: plastic DIL-bent-SIL power package; 17 leads (lead length 12 mm)
SOT243-1


DIMENSIONS (mm are the original dimensions)

| UNIT | $\mathbf{A}$ | $\mathbf{A}_{\mathbf{2}}$ | $\mathbf{b}_{\mathbf{p}}$ | $\mathbf{c}$ | $\mathbf{D}^{(\mathbf{1})}$ | $\mathbf{d}$ | $\mathbf{D}_{\mathbf{h}}$ | $\mathbf{E}^{(\mathbf{1})}$ | $\mathbf{e}$ | $\mathbf{e}_{\mathbf{1}}$ | $\mathbf{e}_{\mathbf{2}}$ | $\mathbf{E}_{\mathbf{h}}$ | $\mathbf{j}$ | $\mathbf{L}$ | $\mathbf{L}_{\mathbf{3}}$ | $\mathbf{m}$ | $\mathbf{Q}$ | $\mathbf{v}$ | $\mathbf{w}$ | $\mathbf{x}$ | $\mathbf{Z}^{(\mathbf{1})}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| mm | 17.0 | 4.6 | 0.75 | 0.48 | 24.0 | 20.0 | 10 | 12.2 | 2.54 | 1.27 | 5.08 | 6 | 3.4 | 12.4 | 2.4 |  |  | 2.1 |  |  |  |
|  | 15.5 | 4.4 | 0.60 | 0.38 | 23.6 | 19.6 | 10 | 11.8 |  |  |  |  | 3.1 | 11.0 | 1.6 | 4.3 | 1.8 | 0.8 | 0.4 | 0.03 | 2.00 |

Note

1. Plastic or metal protrusions of 0.25 mm maximum per side are not included.

| OUTLINE <br> VERSION | REFERENCES |  |  |  | EUROPEAN <br> PROJECTION | ISSUE DATE |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | IEC | JEDEC | EIAJ |  |  |  |
| SOT243-1 |  |  |  |  | $-97-12-16$ |  |

# Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier 

## 17 SOLDERING

### 17.1 Introduction to soldering through-hole mount packages

This text gives a brief insight to wave, dip and manual soldering. A more in-depth account of soldering ICs can be found in our "Data Handbook IC26; Integrated Circuit Packages" (document order number 9398652 90011).

Wave soldering is the preferred method for mounting of through-hole mount IC packages on a printed-circuit board.

### 17.2 Soldering by dipping or by solder wave

The maximum permissible temperature of the solder is $260^{\circ} \mathrm{C}$; solder at this temperature must not be in contact with the joints for more than 5 seconds.

The total contact time of successive solder waves must not exceed 5 seconds.

The device may be mounted up to the seating plane, but the temperature of the plastic body must not exceed the specified maximum storage temperature ( $\mathrm{T}_{\text {stg(max) }}$ ). If the printed-circuit board has been pre-heated, forced cooling may be necessary immediately after soldering to keep the temperature within the permissible limit.

### 17.3 Manual soldering

Apply the soldering iron ( 24 V or less) to the lead(s) of the package, either below the seating plane or not more than 2 mm above it. If the temperature of the soldering iron bit is less than $300^{\circ} \mathrm{C}$ it may remain in contact for up to 10 seconds. If the bit temperature is between 300 and $400^{\circ} \mathrm{C}$, contact may be up to 5 seconds.
17.4 Suitability of through-hole mount IC packages for dipping and wave soldering methods

| PACKAGE | SOLDERING METHOD |  |
| :--- | :--- | :--- |
|  | DIPPING |  |
| DBS, DIP, HDIP, SDIP, SIL | suitable | Suitable ${ }^{(1)}$ |

## Note

1. For SDIP packages, the longitudinal axis must be parallel to the transport direction of the printed-circuit board.

# Power stage $2 \times 50 \mathrm{~W}$ class-D audio amplifier 

## 18 DATA SHEET STATUS

| LEVEL | DATA SHEET STATUS ${ }^{(1)}$ | PRODUCT STATUS ${ }^{(2)(3)}$ | DEFINITION |
| :---: | :---: | :---: | :---: |
| I | Objective data | Development | This data sheet contains data from the objective specification for product development. Philips Semiconductors reserves the right to change the specification in any manner without notice. |
| II | Preliminary data | Qualification | This data sheet contains data from the preliminary specification. Supplementary data will be published at a later date. Philips Semiconductors reserves the right to change the specification without notice, in order to improve the design and supply the best possible product. |
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## Notes

1. Please consult the most recently issued data sheet before initiating or completing a design.
2. The product status of the device(s) described in this data sheet may have changed since this data sheet was published. The latest information is available on the Internet at URL http://www.semiconductors.philips.com.
3. For data sheets describing multiple type numbers, the highest-level product status determines the data sheet status.

## 19 DEFINITIONS

Short-form specification - The data in a short-form specification is extracted from a full data sheet with the same type number and title. For detailed information see the relevant data sheet or data handbook.

Limiting values definition-Limiting values given are in accordance with the Absolute Maximum Rating System (IEC 60134). Stress above one or more of the limiting values may cause permanent damage to the device. These are stress ratings only and operation of the device at these or at any other conditions above those given in the Characteristics sections of the specification is not implied. Exposure to limiting values for extended periods may affect device reliability.

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## NOTES

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NOTES

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